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AERIS RESOURCES LIMITED

TRITTON MINES OPERATIONS

Tritton Deposit

Mineral Resource and Ore Reserve Estimate

30th June 2016

Report Version Rev 00

Author/s	**Name**	**Title**
	Brad Cox	Competent Person – Mineral Resource estimate
	Ian Sheppard	Competent Person – Ore Reserve estimate

1 PROJECT SUMMARY

1.1 INTRODUCTION AND SETTING

The Tritton deposit is a sulphide copper mineralised body located on ML1544 in central New South Wales (NSW), Australia. The deposit geology is described as a Besshi style volcanic associated massive sulphide occurrence. It contains economic grades of copper and silver. Minor gold content in the ore is generally not economic since, after ore processing the gold concentration in copper concentrate is below the payable limit offered by copper smelters.

The deposit is being mined using underground methods by Tritton Resources Pty Ltd a subsidiary of Aeris Resources Limited. The Tritton ore body was discovered in 1995 by a Joint Venture partnership between Straits Mining Pty Ltd and Nord Australex Nominees Pty Ltd.

Mining of the Tritton ore body commenced in 2004 with the development of an access decline and construction of a sulphide ore processing plant. Stope production commenced in March 2005. In its first year of production, Tritton produced 23,088t of copper in concentrate. Production rates are now 23,000t to 24,000t of copper recovered to copper concentrate per annum. Ore is treated at the Tritton copper sulphide ore processing plant by flotation to produce a copper concentrate product. Copper concentrate for the life of mine is sold under contract to Glencore International. Concentrate is transported by from mine by truck and then rail to the port of Newcastle. It is then shipped in 10,000t to 12,000t lots to smelters in the Asia Pacific region.

The Tritton mine is fully permitted for production.

This Mineral Resource and Ore Reserve estimate is an update on previously reported estimates for the Tritton deposit. The previous reported estimate was at 30th June 2015. This updated estimate is based on a resource definition drill program targeting the mineralised system between the 4200mRL to 4000mRL levels (1,070m to 1,270m below surface), it accounts for depletion due to mining and includes data from grade control drilling completed since last estimate.

1.2 LOCATION

The Tritton copper mine is located approximately 45km northwest of the township of Nyngan in central NSW. Nyngan with a population of 3,000 is the regional centre. The small village of Hermidale, population 50, is located approximately 15km to the south of Tritton.

Access to the mine is via the sealed Barrier Highway from Nyngan to Hermidale and then via the sealed Yarrandale road from Hermidale to the mine site.

The deposit is located on ML1544.

1.3 HISTORY

Mining of the Tritton ore body commenced in 2004 with the development of an access decline and construction of a sulphide ore processing plant. Stope production commenced in March 2005. In its first year of production, Tritton produced 23,088t of copper in concentrate. Production rates are now 23,000t to 24,000t of copper in concentrate per annum. Ore mined from the small North East and Larsens underground mines are also processed at the Tritton ore processing plant increasing total plant production up to 30,000t of copper in concentrate per annum. In 2016 development of the Murrawombie underground mine project re-commenced and this production source will replace the exhausted North East and Larsen mine. Murrawombie mine ore will supplement the ore from Tritton mine and sustain the total Tritton Operations production at 28,000 to 30,000t of copper in concentrate in 2016 and 2017.

In 2010, a plant to manufacture cemented paste fill from processing plant tailing was installed. This facilitated a change in mining method that eliminated the requirement to leave pillars behind in the ore body. High percentage extraction of the resource has been achieved since 2011, (typically 80%). Pillars of ore remaining from mining prior to 2010 are still in place and limited recovery of this resource is planned.

Ore production rates have increased over time from 0.8Mt per year to 1.3Mt per year despite mining getting progressively deeper.

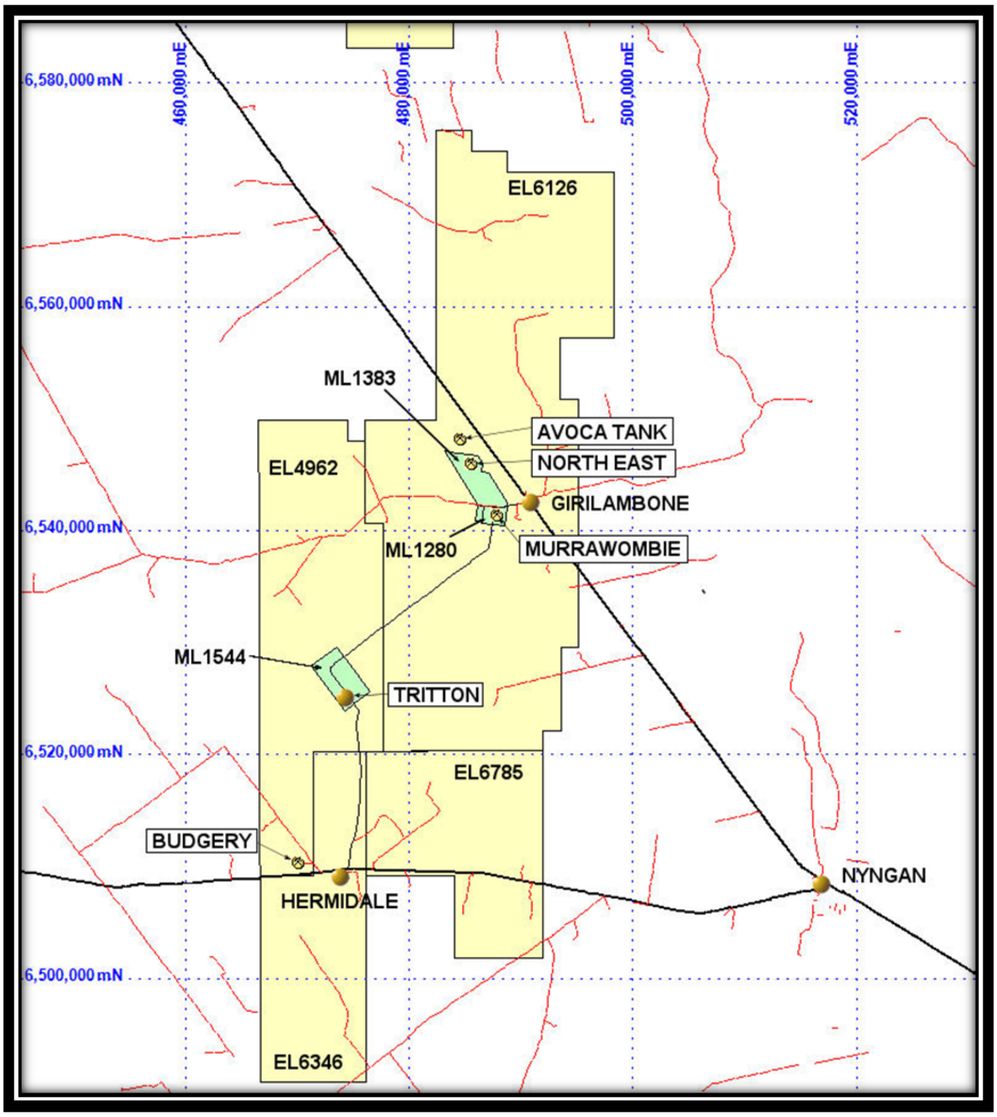


Figure 1 Location and Lease outlines for the Tritton Copper Operation.

2 GEOLOGY

Regionally mineralisation is hosted within early to mid-Ordovician turbidite sediments, forming part of the Girilambone Group. The Tritton mineralisation is hosted within greenschist facies, deformed pelitic to psammitic sediments, and sparse zones of coarser sandstones.

The Tritton sulphide mineralisation is stratiform and is classified as a “Besshi style” volcanogenic massive sulphide. Mineralisation is dominated by banded to stringer pyrite – chalcopyrite, with a relatively consistent massive pyrite – chalcopyrite unit along the hanging wall contact. Alteration assemblages adjacent to mineralisation are characterised by an ankerite/chlorite footwall and silica sericite hanging wall. The mineralisation has been variably folded at periodic intervals throughout the resource.

2.1 RESOURCE ESTIMATION MODEL

The reported resource estimates for the Tritton deposit are derived from an updated geology interpretation and block model completed in February 2016.

Copper mineralisation is constrained within a bounding 0.4% copper grade shell. Internally within this wireframe two unmineralised turbidite sequences have been modelled separately to ensure mineralisation does not extend into these areas. A thin ≤ 5m HW massive pyrite with variable chalcopyrite horizon was also modelled separately. The massive sulphide horizon moves within and outside of the main 0.4% copper shell and was important to constrain mineralisation outside of the bounding 0.4% copper shell.

Drill hole data used in the updated Mineral Resource include a combination of grade control and resource definition drill holes. All drill holes are diamond core with a majority of hole diameters NQ2 size with lesser HQ3 (surface resource definition program completed between 2010 to 2012) and LTK60 (grade control up holes).

All samples are diamond half core and assayed at the ALS Orange laboratory. Copper assays were determined via a three stage aqua regia digestion with an ICP finish (ME-ICP41) and copper assays greater than or equal to 1% were re-submitted for an ore digest (ME-OG46) which is suitable for accurately determining copper grade above 1%. Gold assays were determined via fire assay with an AAS finish using a 30g sample (Au-AA22) suitable for grade ranges from 0.001 g/t Au – 10g/t Au. Samples returning a gold grade at or above 1 g/t Au are resubmitted for an ore grade gold assay (Au-AA25) suitable for grade ranges up to 100 g/t Au. Higher grade gold assays at Tritton are in the order of 10 g/t Au to 30 g/t Au which is well within the detection range.

The resource estimate has been classified and includes Measured, Indicated and Inferred Mineral Resources. A summary of the criteria used to define each category is summarised below:

- Classified Measured Mineral Resource is based on the grade control drilling data defined by a nominal 20m x 20m drill spacing along with underground cross cut samples. Data collected from underground mapping and sludge holes were used to improve the accuracy of geology and estimation domains. Measured Mineral Resource is reported down to the 4170mRL level.
- Classified Indicated Mineral Resource is based on resource definition drilling on a nominal 40m x 40m drill spacing. The geological understanding is sufficient to have a good understanding of geological continuity between drill holes whilst grade intervals provide a reasonable approximation of the global grade. Indicated Mineral Resource is reported between 4170mRL to 4000mRL. A small quantity of additional Indicated Mineral Resource is reported from remnant pillars in the Tritton upper levels (4655mRL to 4565mRL).
- Classified Inferred Mineral Resource is based on resource definition drilling up to a 100m x 100m drill spacing. Two separate zones of Inferred resource have been classified in the updated estimate. The down dip extension of the main Tritton mineralised system contains a majority of the Inferred material between 4000mRL to 3860mRL. In additional a thinner along strike extension of the Tritton mineralised system is also classified as Inferred. This mineralised body appears to be spatially located in the HW of the main Tritton deposit.

Refer to Figure 2 and Figure 3 which outlines the location of the classified Mineral Resource used for the reporting of the Tritton Resource as at 30th June 2016.

Mineralisation remaining above the mining front surface as at 30th June 2016 has been depleted, except for the material in the upper level secondary pillars and thinner along strike extension of Inferred Mineral Resource. All other remnant blocks of mineralisation remaining around mined out areas are not classified as Mineral Resource, (not economic for extraction).

2.2 MINERAL RESOURCE CUT-OFF GRADE

A bounding 0.4% copper grade shell is used to constrain grade estimates for the Tritton deposit. A 0.4% copper cutoff grade was selected based on log probability plots of copper mineralisation within and surrounding the Tritton system. Within the bounding shell other estimation domains include a low grade “internal dilution” and a massive sulphide HW domain. Each estimation domain is based on drill hole assay data and ore textures. Block grades are interpolated within each domain using ordinary kriging.

Within the bounding 0.4% copper grade shell Mineral Resource is reported at a block cut-off grade of 0.6% copper. Mineral Resource is quoted as material at or above a 0.6% copper block cut-off grade. Application of this cut-off grade excludes blocks below 0.6% copper that exist within the grade shell.

In stope design the whole of the 0.4% copper resource domain volume is available for consideration. Engineers will avoid inclusion of low grade blocks from the stope design where possible. However in order to achieve practical stope design it is sometimes necessary to include blocks that are below 0.6% copper inside the stope volume, some stopes will extend outside the resource domain. Thus stopes will often include some material that has not been classified as Mineral Resource, although the volume of this material is small.

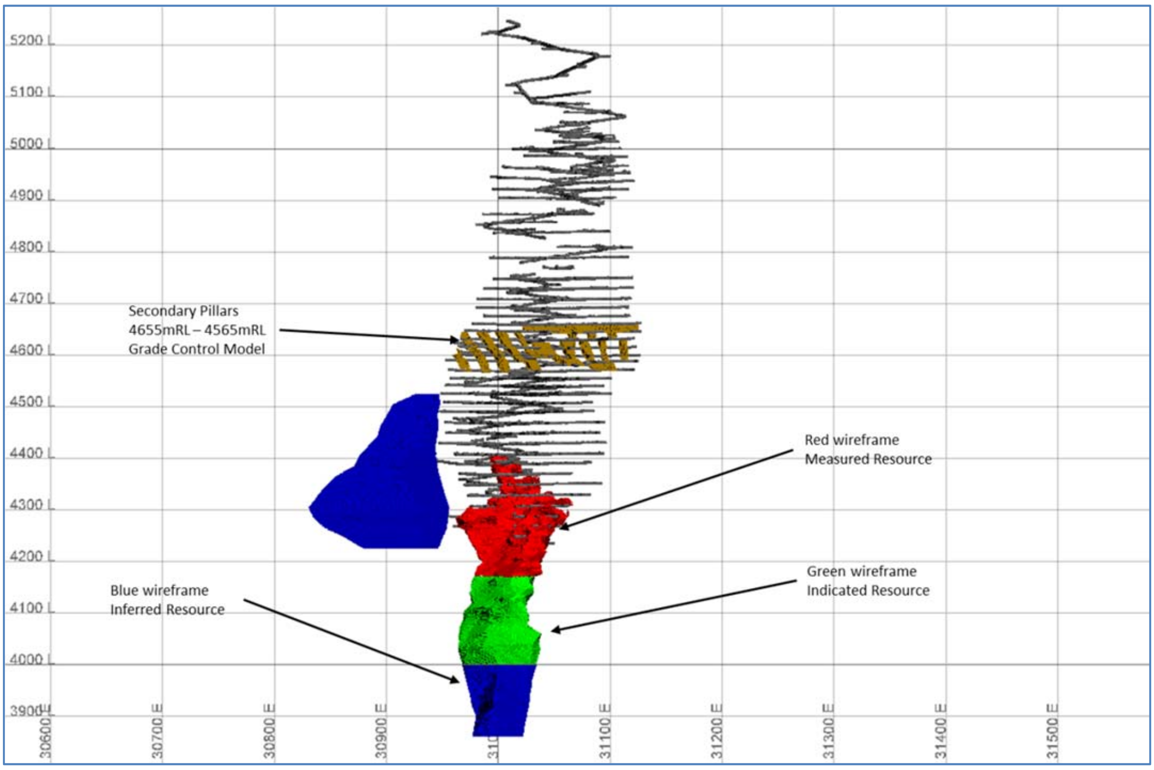


Figure 2 Long section view looking west at the reported Tritton Mineral Resource as at 30 June 2016.

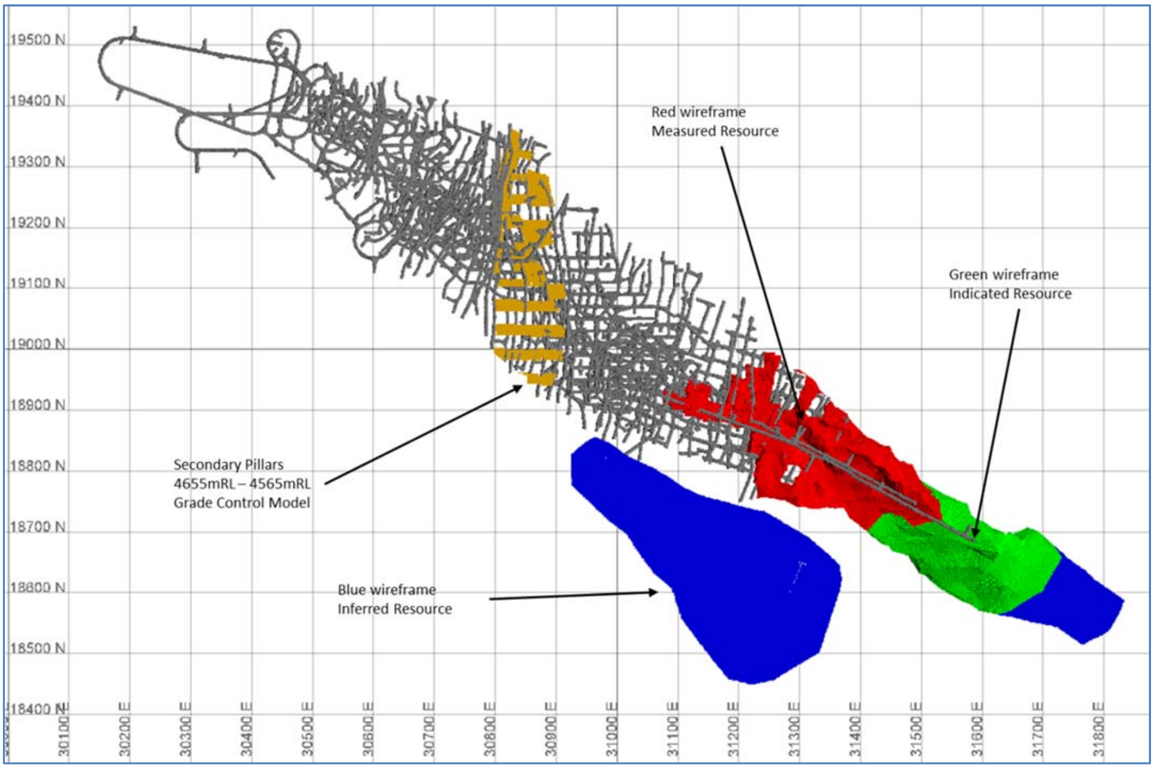


Figure 3 Plan view showing the spatial location of the reported Tritton Mineral resource as at 30 June 2016.

3 MINING

3.1 MINING METHOD

Mining method used at Tritton mine is sublevel open stoping or retreating bench stoping. Transverse or longitudinal stope orientation is used depending on the geometry of the ore lenses.

Stopes are backfill with cemented paste fill made from mill tailing. Use of paste fill provides support of the ground around mined out stopes. Mineral Resource recovery is typically over 80% since the use of cemented paste fill means there is no requirement to leave permanent pillars for ground support.

Stopes are mined between sub-levels separated 20m vertically, (floor to floor). Stope height varies from 20 to 80m depending on the local geometry and hanging wall stability. Stope size increases below 4100mRL in response to changes in the deposit geometry. The mineralisation is generally thicker at depth, so taller stope designs are possible.

Mining is sequenced as top downwards, relying on cemented paste backfill of the upper stopes for hanging wall stability. Stope designs have evolved with the changing deposit geometry. Up to approximately 2014 the stopes were designed to be undercut as mining progressed down dip, relying on high strength paste backfill for stability. Extraction of stopes by horizontal undercut of the cemented backfill in above stope is now avoided, except in narrow areas. Stopes are now designed to extract the ore body from footwall to hanging wall over the full height. The majority of backfill exposures are now near vertical walls adjacent to the down dip stope. Backfill dilution of the ore has been reduced as a result.

Stope designs will include low grade mineralisation, (some small volumes from outside the Mineral Resource envelope), when necessary to achieve a practical mining design. This internal dilution is reported as part of the Ore Reserve. We quote dilution and ore recovery factors as additional to this internal dilution.

Portions of the Mineral Resource that cannot be included in viable stope designs due to thickness or dip are excluded from the Ore Reserve. These portions are progressively depleted from the Mineral Resource as not recoverable.

The Ore Reserve is supported by engineered stope designs that have been individually reviewed for practicality and economic viability. Stope optimizing software, (MSO), is used to assist with the design process, however the volumes generated by this software are not considered suitable for use as Ore Reserve without further engineering design.

3.2 ORE RESERVE CUT OFF GRADE

Copper grade (% Cu) is applied as the only cut-off grade criteria.

Gold content of the ore is not sufficient to be of economic significance to cut-off grade decisions. Silver content of the ore varies in direct proportion with the copper % and so is adequately represented by the simple copper cut-off grade.

A whole of stope cut-off grade of 1.1% copper is applied to the diluted stope grade, (i.e. after dilution and ore loss factors are applied).

Development in ore is designed for each level of the mine as part of the Ore Reserve process. The development design is converted to a solids volume. An estimate of development (or “Jumbo”) ore is made by interrogating the geology block model within this development design solid. Design development solid volumes are excluded from the stope volumes.

No dilution and no ore loss factors are allocated to development ore. All the Mineral Resource within the design development is reported as development ore. This is consistent with mine practice where material down to an estimated grade of 0.5% Cu can be assigned as ore, once broken in a development heading. The net effect is that the cut-off grade for Ore Reserve derived from design development volumes is the same as the Mineral Resource cut-off grade, i.e. 0.6% Cu.

Selected stopes with average grade as low as 0.9% Cu may be included in the Ore Reserve where they can be taken at lower cost in the mining sequence and after evaluation indicates they will be economic. The 2016 Ore Reserve estimate does not include any stopes in this category.

3.3 ORE RESERVE FACTORS

Factors to account for dilution and ore loss are applied in the estimate of Ore Reserve. The factors vary with the size of design stope. Small stopes are defined as those with a vertical height of less than 40m. Tall stopes are those with a vertical height of 40m or more.

Factors applied to small stopes in the estimation of Ore Reserve are 90% ore recovery and 11% dilution. These simple factors give an estimate that is the consistent with reconciliation and stope survey data, within precision of the reserve estimate. Estimates of over and under break and of broken ore that cannot recovered from stope due to oversize rocks or lost in corners that cannot be effectively bogged, based on survey and reconciliation data are presented in the table below. The “insitu grade” is the estimated grade of the volume from interrogation of the geology block model before any factors are applied. “Diluted grade” is the stope ore grade after dilution is estimated. The grade of under break is much higher than the low grade in hanging wall dilution.

Table 1 Estimates of dilution from reviews of stope survey data.

Item	% of Design	Cu%	Ag ppm
Over break – insitu material from hanging wall	12%	0.80%	3.0
Over break – paste from side wall and undercut	3%	0	0
Under break – insitu ore not broken on footwall or stope corners.	12%	Insitu grade	Insitu grade
Unrecoverable broken stocks	2%	Diluted grade	Diluted grade

Factors applied to tall stopes in the estimation of Ore Reserve are 95% ore recovery and 5% dilution. No tall stopes have been mined to date, so no reconciliation information is available. The plan area of small and tall stopes is similar and if hanging wall dilution is relatively constant the relative dilution and ore loss will reduce with tall stopes as function of total stope volume being greater. Tall stopes also have trough design at the bottom draw point level that will improve ore recovery compared to the flat bottom design of the small stopes.

Recovery of pillar stopes from older and shallower areas of the mine, (4465mRL to 4640mRL) form part of the Ore Reserve. Due to the age of pillars and uncertain geotechnical rock mass condition an ore recovery factor of 50% and dilution factor of 20% are applied in the estimate of Ore Reserve. The pillar Ore Reserve is 270kt or 2% of total by tonnage.

Proved and Probable stopes are generally assigned the same dilution and ore loss factors. As a stope design improves with the progression from a conceptual design, (Probable status) to final design. (Proved status) the ore grade tends to improve and tonne can vary either up or down. There is no evidence to suggest the need for different factors applied to different category of Ore Reserve.

3.4 RECONCILIATION DATA

Reconciliation against stopes mined in 2015 indicate that the ore reserve estimation factors are slightly conservative, consistent with results for previous years.

Table 2 2015 stope reconciliation data

	Ore Tonne	Grade %Cu	Copper Tonne
Ore Reserve with factors;11% dilution and 90% recovery	1,133,113	1.88	21340
Reconciled against stope survey and geology model	1,159,154	1.96	22763
Reconciled against mill final production	1,116,828	1.86	20808

3.5 CLASSIFICATION

Ore Reserves are classified as Proved or Probable based on conversion from Measured and Indicated Mineral Resources respectively. Individual stope designs are reviewed and classification may be down - graded from Proved to Probable where there is high risk of ore production being lower than estimated. The upper level pillar stopes have been classified as Probable Ore Reserve under this process. There are no other areas where significant down grading to Probable has occurred.

Figure 4 Tritton mine section showing surface portal to base of Ore Reserve, (4050mRL)

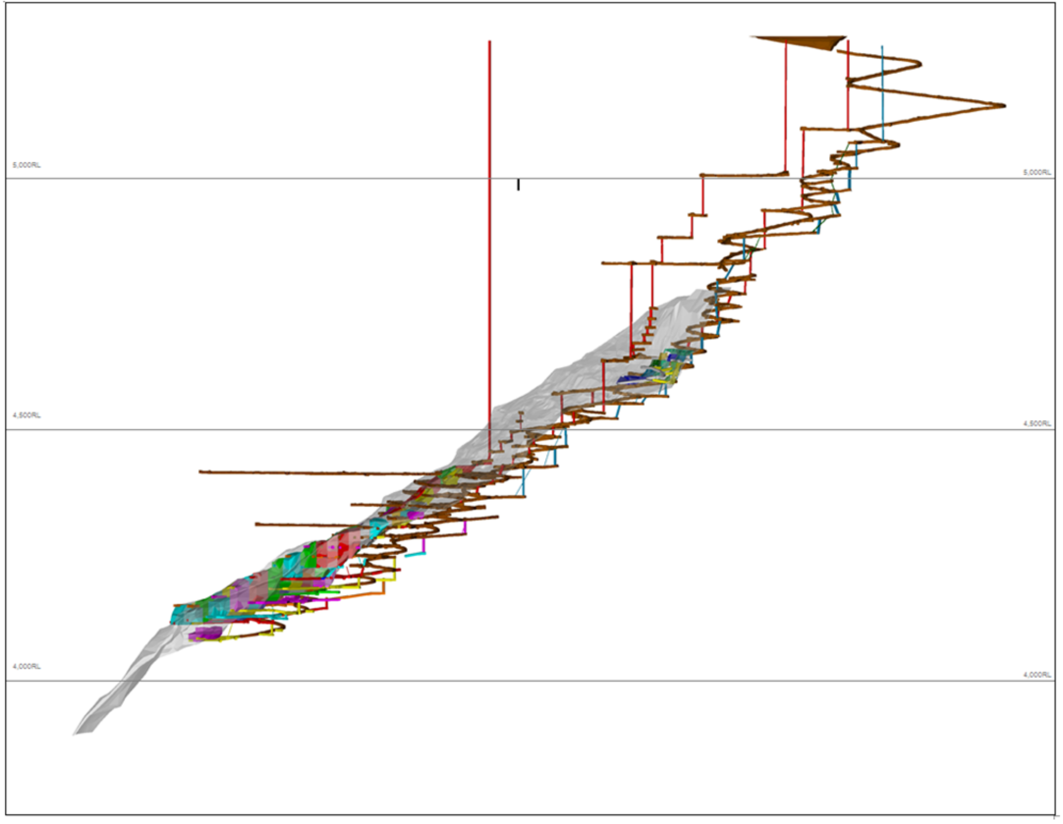
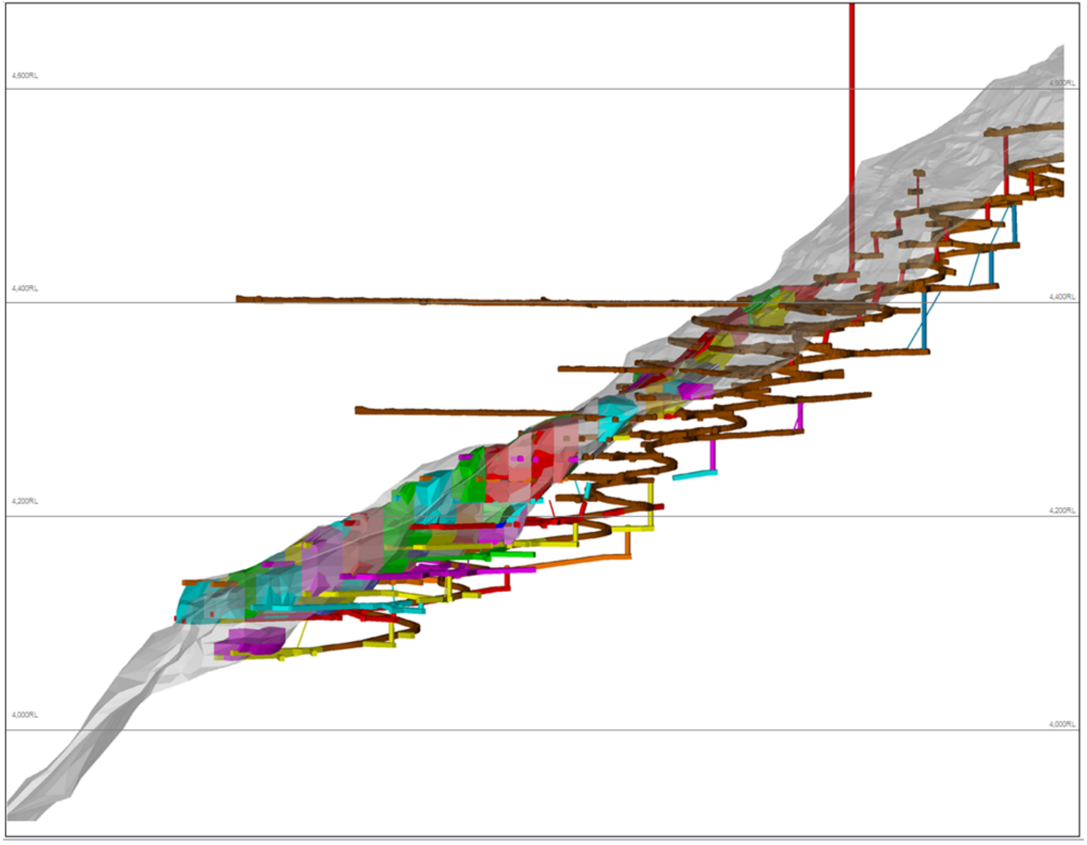


Figure 5 Tritton mine section showing lower levels



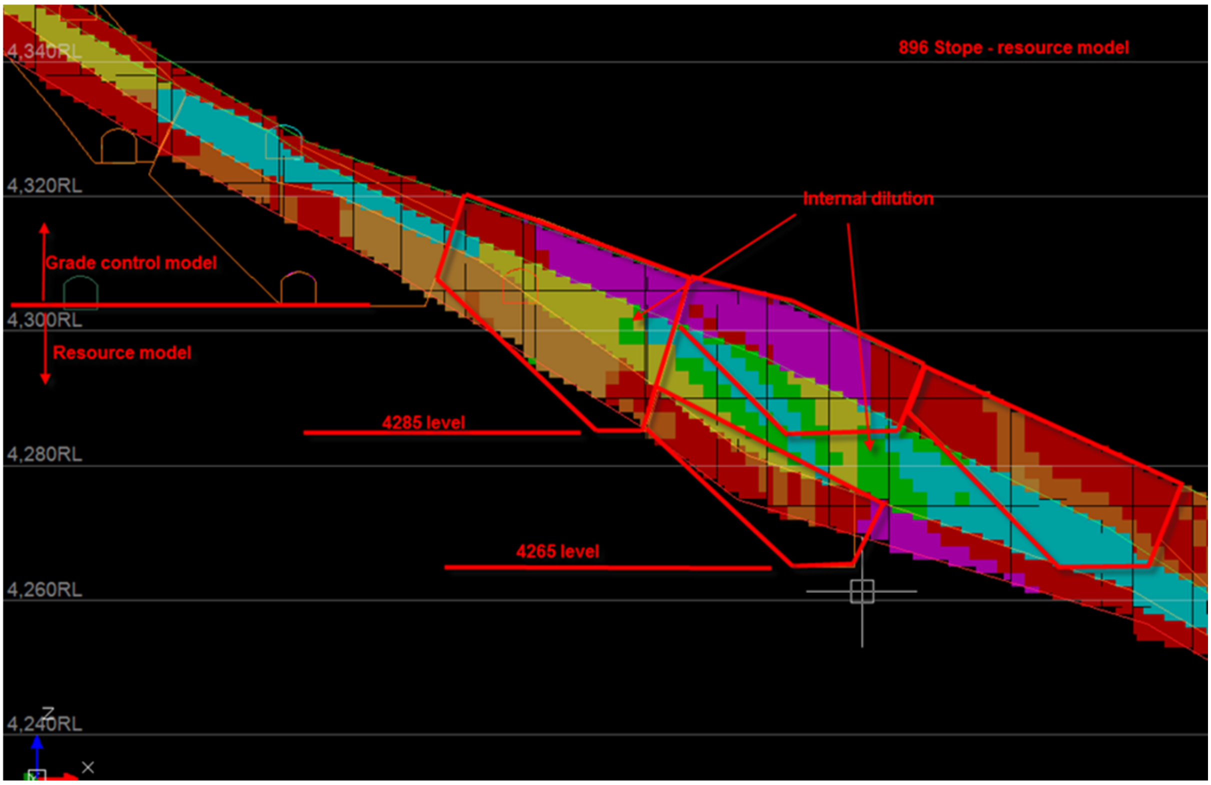


Figure 6 Typical cross section showing stope design higher grade lens on hanging wall and footwall with internal low grade zone.

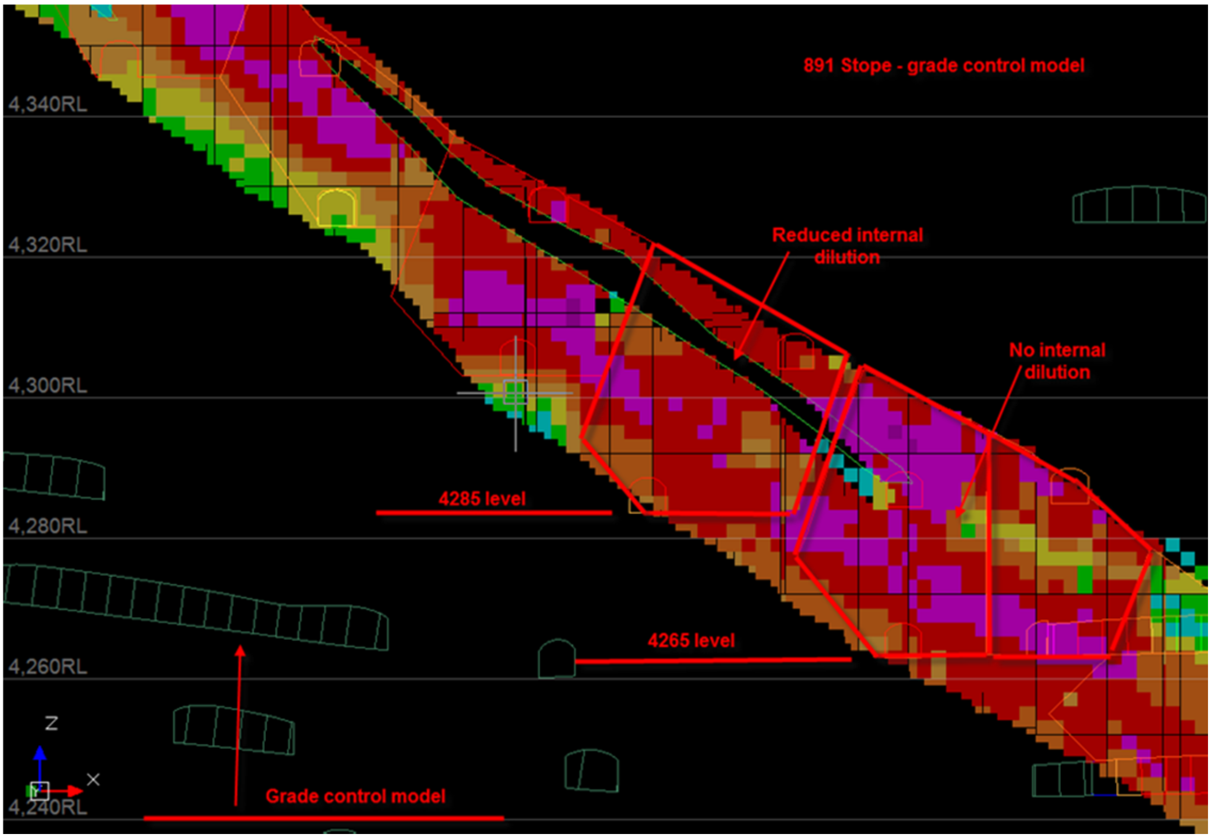


Figure 7 Typical section showing typical small stope design.

4 ORE PROCESSING

The ore produced from the Tritton mine is processed at the Tritton copper sulphide ore processing plant. Copper, silver and gold is recovered by crushing, grinding and conventional flotation of sulphides to produce a copper concentrate.

The copper concentrate product is clean with no impurities that attract a penalty from smelters. The high quality Tritton concentrate is sought after by smelters in the Asia Pacific region.

Copper recovery of 94 to 95% has been consistently achieved at 24% copper grade in concentrate for many years of operation. There are no indications of a change in geology at depth that is likely to change the quality of future copper concentrate.

Published Mineral Resource and Ore Reserves do not include an estimate of the silver grade since it is not modelled to sufficient precision and it has modest economic impact. The average silver grade in Tritton ore is 6g/t and this recovers to a silver in copper concentrate of approximately 60g/t that is payable by the smelters at 90%. This has a modest value of $40 to $50/t of concentrate.

Published Mineral Resource and Ore Reserves do not include an estimate of the gold grade since it has minimal economic impact on the mine. Average gold grades of 0.14g/t recover to approximately 0.8g/t in the copper concentrate. This is below the 1.0g/t payable limit for copper concentrate. An occasional shipment of copper concentrate is produced that contains above the 1.0g/t gold content, however the economic impact is small. Gold is ignored in the Ore Reserve estimate.

Mill tailing is disposed to either the underground stopes as paste backfill (approximately 30 to 40% of the total tailing) or to the Tritton tailing storage facility. The tailing storage facility has at least sufficient capacity to hold an additional eight (8) years tailing production at forecast processing rates. This is more than sufficient to cover this Ore Reserve estimate.

5 ECONOMIC STUDIES AND APPROVALS

The Mineral Resource and Ore Reserve estimate is supported by both a detailed operations budget and a life of mine plan that demonstrate the economic viability of the mine. The Tritton mine is operating and has been operating continuously for ten years. Operating costs, and mine production rates are estimated with a level of confidence that exceeds a feasibility study expectation. Reconciliation of production demonstrates that estimation of the Mineral Resource can be made with confidence that exceeds the expectation of a feasibility study.

Copper and gold prices used for estimation of revenue for the purposes of Ore Reserve and Mineral Resource estimation are Aeris Resources assumptions based on consensus pricing information from market analysts, banks and financial institutions. These prices change over the life of the mine. The mid-life price assumptions applied in the estimate are;

- Copper price of USD$5,200/tonne;
- Gold price of USD$1200/oz;
- Silver price of USD$17/oz;
- AUD:USD exchange rate of 0.71;
- Copper treatment charge of USD$100/tonne copper concentrate;
- Copper refinery charge of USD10c/lb copper.

Tritton Resources holds all necessary approvals from the State to carry out mining operations at Tritton mine and the associated Tritton ore processing plant.

6 MINERAL RESOURCE ESTIMATE

6.1 RESULTS

The Mineral Resource estimate reference date is 30th June 2016. The Tritton deposit has been mined and the Mineral Resource depleted since the previous public report.

Table 3 Classified Mineral Resource for the Tritton deposit as at 30th June 2016 [1,2,3,4,5]

Resource Category	Tonne (kt)	Copper (%)	Contained Copper (kt)
Measured	3,850	1.9	73
Indicated	5,430	1.4	73
Total M&I	**9,270**	**1.6**	**146**
Inferred	1,960	1.2	24
Total	**11,240**	**1.5**	**169**

1. Mineral Resources are quoted as INCLUSIVE of Ore Reserve.
2. Mineral Resource is reported at a 0.6% Cu cutoff grade.
3. Discrepancy in summation may occur due to rounding.
4. Estimate is constrained by the survey stope and development positions for Tritton as at end June 2016.
5. Indicated estimate includes 490k tonne at 2.6% Cu for 12.7 k tonne of copper metal contained in the upper Tritton Pillars between the 4655m RL and 4565m RL that have been down-graded from Measured Resource due to risk.

6.2 CHANGE FROM PREVIOUS PUBLIC REPORT

Material changes to the Tritton Mineral Resource from the previous reporting period include mine depletion, additional drilling data resulting in spatial changes to the mineralised system and a revised geological interpretation. Mine production in the period reported between each model from end June 2015 to end June 2016 was 1,412 thousand tonne at 2.0% copper for 27.6 thousand tonne contained copper. This production depleted the Mineral Resource. Net depletion of the Mineral Resource is different from mine production due to the combined impact of dilution and ore loss during mining as well as variation between estimated and actual Mineral Resource.

The updated resource model has changed noticeably in comparison to the previously reported Mineral Resource which was created in 2012. The differences relate to an increase in drill density and spatial changes to the mineralised system through the previous Indicated and Inferred regions. Additions to the mineralised system are associated with the increased thickness and geometry changes at depth below 4200mRL and extensions to the known mineralised system below 4000mRL.

Table 4 Change in the reported Tritton Mineral Resource since previous public report

Estimate	Resource Category	Tonne (kt)	Copper (%)	Contained Copper (kt)
June 2016	Measured	3,850	1.9	73
	Indicated	5,430	1.4	73
	Total M&I	**9,270**	**1.6**	**146**
	Inferred	1,960	1.2	24
	Total	**11,240**	**1.5**	**169**
June 2015	Measured	2,750	2.1	59
	Indicated	4,620	1.7	79
	Total M&I	**7,380**	**1.9**	**138**
	Inferred	3,140	1.4	45
	Total	**10,520**	**1.7**	**182**
difference	Measured	1,100	-0.2	14
	Indicated	810	-0.4	-6
	Total M&I	**1,890**	**-0.3**	**8**
	Inferred	-1,180	-0.2	-21
	Total	**720**	**-0.2**	**-13**

Figure 8 Tonnage changes between the June 2015 and June 2016 Tritton reported figures (including Tritton pillars).

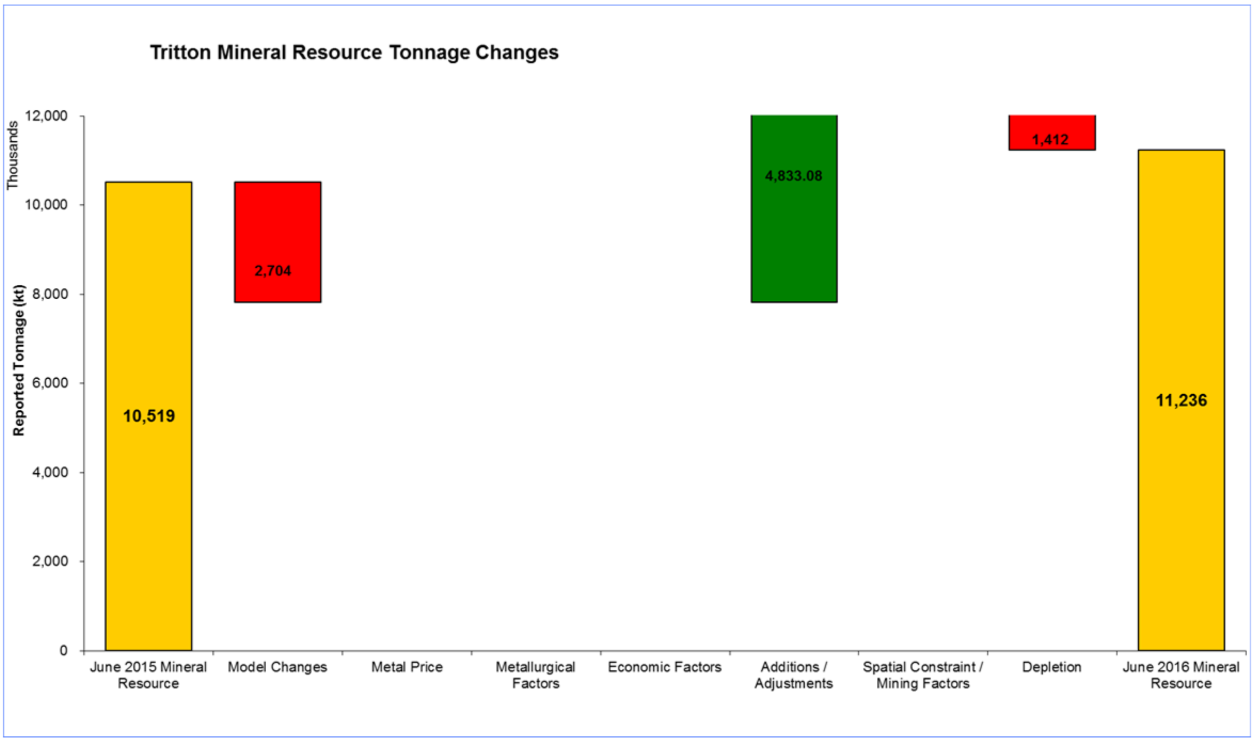


Figure 9 Copper metal changes between the June 2015 and June 2016 Tritton reported figures (including Tritton pillars).

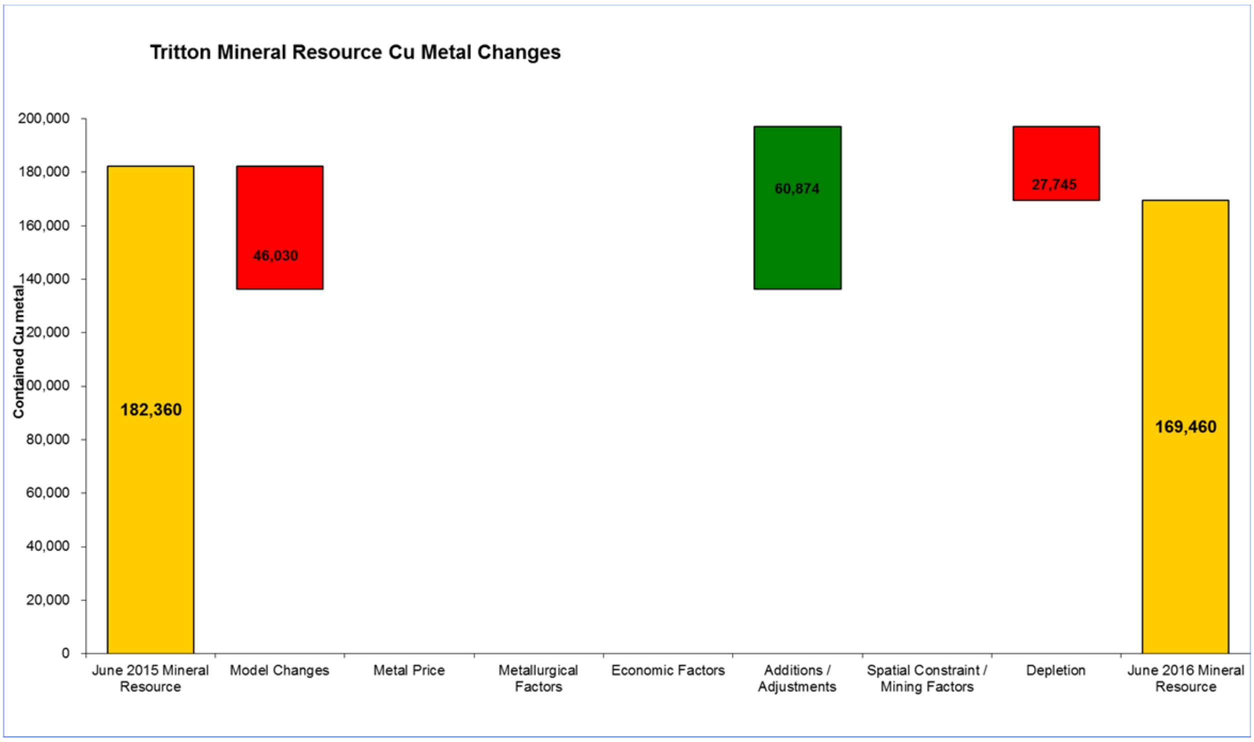
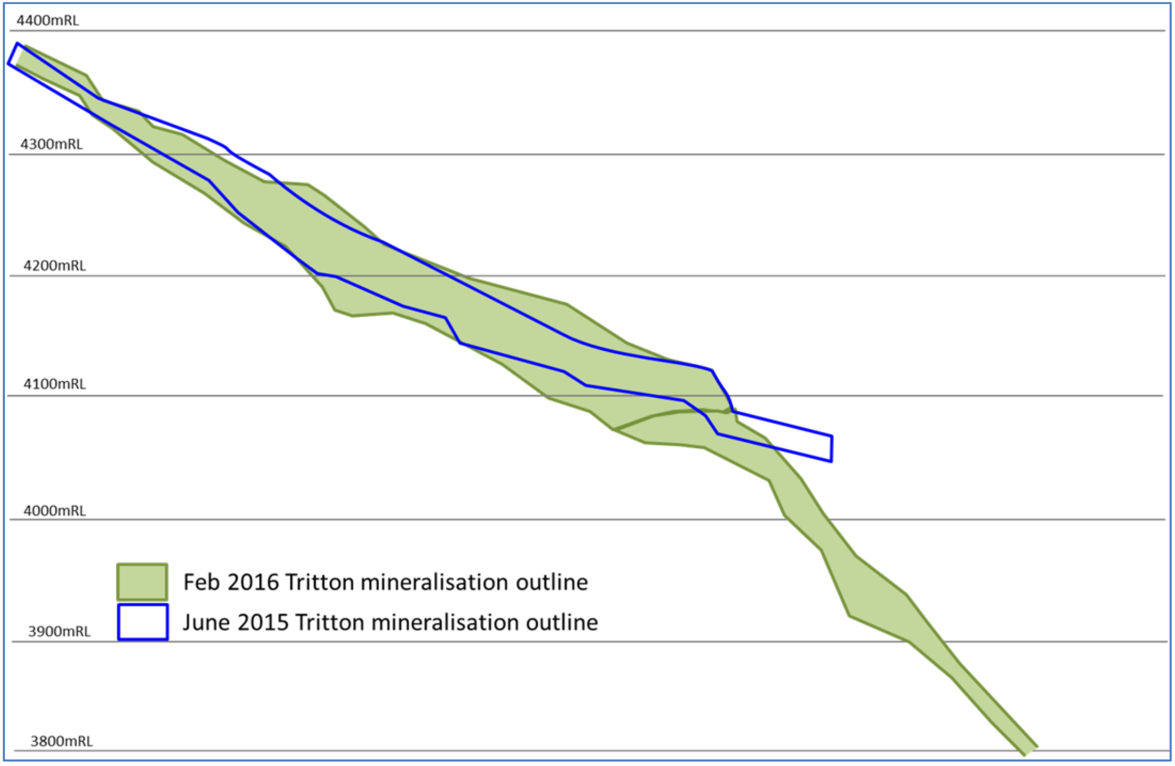


Figure 10 Cross section looking north through the Tritton mineralised system showing the outline of the bounding 2012 and 2016 grade shells.



6.3 STATEMENT OF COMPLIANCE WITH JORC CODE REPORTING

This Mineral Resource statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves.

6.3.1 Competent Person Statement

I, Brad Cox confirm that I am the Competent Person for the Tritton Mineral Resources section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having relevant experience to the style of mineralisation and type of deposit described in the Report and to the activity for which I am accepting responsibility.
- I am a Member of the Australasian Institute of Mining and Metallurgy, (AusIMM membership No.220544).
- I have reviewed the Report to which this Consent Statement applies.

I am a full time employee of Aeris Resources Limited.

I verify that the Tritton Mineral Resource section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to Mineral Resources.

6.3.2 Competent Person Consent

With respect to the sections of this report for which I am responsible – Mineral Resource Estimate - I consent to the release of the Tritton Mineral Resources and Ore Reserves Statement as at 30th June 2016 by the directors of Aeris Resources Limited.

Signature of Competent Person Brad Cox, AusIMM member 220544 Bradley Co.	Date 21st July 2016
Signature of witness	Name and address of witness Narelle Wynn Lutwyche Q 4030

6.4 JORC CODE, 2012 EDITION – TABLE 1 REPORT: TRITTON MINERAL RESOURCE

6.4.1 Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	*1. Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* *2. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* *3. Aspects of the determination of mineralisation that are Material to the Public Report.* *4. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	1. All Diamond core samples are based on ½ core. Pre-collar RC samples in waste zones taken as 4 metre composites and re-spit to 1 metre samples when return assays or geology indicate copper or gold mineralisation. Underground samples are collected from drive headings or cross cuts at 1 metre intervals or at geological breaks. Underground samples are collected as rock chips. 2. All diamond core is aligned, measured and metre marked. All underground face samples are digitally photographed with face positions measured from survey control points and survey pickups. Underground cross cuts are not digitally photographed however their positions are referenced from survey control points. 3. During all drill programs at the Tritton deposit Aeris Resources have ensured drill contractors completing the works maintain a high industry standard. Diamond drill sample lengths are generally taken at 1.0 metre intervals. At geological boundaries (based on mineralisation textural differences or material changes in chalcopyrite content) the sample length can vary between a minimum of 0.5 metres and maximum of 1.4 metres. Sampling is extended 10m beyond the mineralised system. Exploration and resource definition diamond core drilled from surface which intersected the mineralised Tritton deposit pre 2010 are predominantly NQ2 in size. Resource definition holes drilled during 2010 to 2012 (targeting 4300mRL to 4000mRL) are HQ3 in size while resource definition holes drilled from 2014 onwards (4200mRL to 3900mRL) are NQ2 in size. Underground grade control holes are NQ2 for down holes and LTK60 for up holes. Underground face samples (rock chip) are also collected for grade estimation with ore drives mapped and ore boundaries

Criteria	JORC Code explanation	Commentary
		picked up by survey. All Exploration holes sampled by Aeris Resources for the Tritton Mineral Resource are analysed by a 35 element three stage Aqua Regia digestion with an ICP finish (ME-ICP41) suitable for Cu concentrations between 1 ppm to 10,000 ppm. All Cu samples greater than or equal to 1.0% Cu were re-submitted for an ore digest to determine Cu concentrations greater than 1.0% (ME-OG46). Au assays were completed via fire assay fusion with an AAS finish using a 30g charge (Au-AA22) suitable for Au grade ranges between 0.001 g/t – 10 g/t. All Au samples greater than or equal to 1.0 g/t Au were re-submitted for an ore grade 30g fire assay charge to determine Au concentrations greater than 1.0 g/t Au (Au-AA25). All grade control diamond drill holes and underground samples are assayed using the ore grade digest method (ME-OG46) for Cu, Fe, Ag, Zn, Pb and S. Au assays are completed via Au-AA25. Sample preparation and assaying are completed at the ALS laboratory in Orange N.S.W.
Drilling techniques	*1. Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	1. All drilling data intersecting the Tritton mineralised system was completed via diamond drilling. A small number of RC drill holes were completed early in the exploration phase pre 2000. These drill holes targeted up upper portions of the mineralised system which has subsequently been mined. Diamond hole diameter sizes vary from HQ3 and NQ2 for resource definition programs. Grade control hole diameter sizes are NQ2 for down holes and LTK60 for up holes. All underground samples are rock chip samples.
Drill sample recovery	*1. Method of recording and assessing core and chip sample recoveries and results assessed.* *2. Measures taken to maximise sample recovery and ensure representative nature of the samples.* *3. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	1. All diamond core recoveries are measured and recorded by Aeris Resources field technicians or geologists. Initial drill holes completed by NORD targeting the Tritton deposit did not have RQD routinely recorded (BDS006 to BDS125). RC pre-collar sample recoveries were not recorded nor required to be recorded as all material estimated for the Tritton mineralisation is defined by diamond drill core. RQD measurements are taken on all core prior to all sampling. This procedure has been part of

Criteria	JORC Code explanation	Commentary
		the standard drill core processing procedure since 2005. 2. Rock competency is very good through the Tritton mineralised system and adjoining country rock. Faults intersected are generally sub metre in thickness and contain minor amounts of clay/fine susceptible to core loss. Industry standard drilling practices are maintained to ensure sample recoveries and core presentation remains at a high level. 3. No significant relationship appears to exist between recovery and grade.
Logging	*1. Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* *2. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.* *3. The total length and percentage of the relevant intersections logged.*	1. All diamond core and RC chips are geologically logged by company geologists. All surface holes drilled by Aeris Resources are geotechnically logged. All logging is to the level of detail to support the Tritton style of mineralisation (VMS Besshi style). 2. Logging of diamond core and RC samples record lithology, alteration, mineralisation, degree of oxidation, structure, RQD and recovery. All exploration core was photographed in both dry and wet form. Underground resource definition and grade control holes are photo in wet form only. All RC intervals are stored in plastic chip trays, labelled with intervals and hole number. Core is stored in core trays and labelled similarly. Underground headings which have been sampled are spatially referenced using survey control points. Underground headings which are sampled have a digital photography taken. 3. All RC and core samples were logged in full. Underground samples are logged for lithology and structure.
Sub-sampling techniques and sample preparation	*1. If core, whether cut or sawn and whether quarter, half or all core taken.* *2. If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.* *3. For all sample types, the nature, quality and appropriateness of the sample preparation technique.* *4. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.*	1. Diamond core samples are cut using an Almonte automatic core saw. Half core samples are collected on average at 1.0 m intervals and can vary between 0.5 metres to 1.4 metres. Sample intervals not equal to 1.0 metre generally occur at mineralisation/geology contacts. 2. RC samples for waste sections are collected at 1 metre intervals, with a 1m split and bulk residual collected on the drill rig. The bulk residual was composited to 4 metre intervals by spear

Criteria	JORC Code explanation	Commentary
	5. *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* 6. *Whether sample sizes are appropriate to the grain size of the material being sampled.*	sampling. If RC composites returned above background copper or gold values, the stored original 1m split was sent to the laboratory for analysis. 3. Samples taken are appropriate for the Tritton mineralisation style (Copper VMS). Half core drill core samples are sent to ALS laboratory in Orange for sample preparation and assaying. Upon arrival at the laboratory sample weights are recorded. Samples greater than 3kg are crushed via a Boyd crusher (90% passing 2mm) and rotary split to a sub sample between 2kg to 3kg. The sub sample is pulverised via a LM5 to 85% passing 75µm. A 300g sample is taken from the pulverised material for assaying. Samples less thank 3kg are crushed via a jaw crusher to 70% passing 6mm and the whole sample is pulverised in a LM5 with a 300g sub sample taken for assaying. Underground face samples are treated in the same manner as diamond core described above. 4. Sample blanks and industry standards are routinely submitted at a frequency of 1:20. Duplicates and Pulps are retained and re-submitted periodically to test assay reproducibility. 5. Field duplicates from grade control holes are conducted routinely. Regression analysis of the field duplicates shows very good correlation. The understanding of sample representativeness and grade estimation is also reviewed through mine to mill reconciliations and stope reconciliations and closing reports. All core samples are visually examined against assay values and logged mineralisation. 6. The sample sizes are considered appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	1. *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* 2. *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	1. Mineralisation at the Tritton deposit is associated with primary sulphides. Copper mineralisation is primarily associated with chalcopyrite. Copper mineralisation is largely interpreted to be remobilised and varies in nature from fine disseminated spots to zones of erratic +10cm scale stockwork textures. The assay methods described previously are considered appropriate for the style of mineralisation. Sample preparation methods are also

Criteria	JORC Code explanation	Commentary
	3. Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	considered appropriate for the style of mineralisation. Review of sample duplicates indicates the assay repeatability is very good. 2. Information regarding assay techniques used for samples taken pre 2005 cannot be confirmed. However drill holes completed up to this period are associated with mineralised zones which have already been mined. Aeris Resources are confident the assay methods used would meet industry standards based on the geological protocols in place at the time. 3. No other methods were used to derive assay values for resource estimation. 4. Laboratory QA/QC samples included the use of blanks, duplicates, standards (commercial certified reference materials) and repeats.
Verification of sampling and assaying	*1. The verification of significant intersections by either independent or alternative company personnel.* *2. The use of twinned holes.* *3. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* *4. Discuss any adjustment to assay data.*	1. Significant mineralised intersections are reviewed by the logging geologist. QAQC results are reviewed on a batch by batch and monthly basis. Deviations from precision tolerances are investigated on a batch by batch basis. If grade bias is observed then follow up with the laboratory typically occurs on a monthly basis. 2. No twinned holes were conducted. 3. All Aeris Resources geological data is logged directly to a Panasonic tough book laptop at the core yard using company logging codes. Data is logged directly to Acquire (off line) which is then uploaded to the Acquire network database once the computer is docked to the office workstation. In built Acquire validation occurs at the time of data entry. Assay results are returned electronically on a batch by batch basis from the ALS laboratory via the webtrieve portal. Returned assay batches are reviewed prior to upload to the Acquire database. If a batch fails QAQC procedures then follow up and potential reassaying from the laboratory is required. Assay data are not uploaded to the Acquire database until a batch passes all QAQC tests. 4. No adjustments to assay data are made.
Location of	*1. Accuracy and quality of surveys used to locate drill holes (collar*	1. All surface drill holes completed from 2005 onwards have collar

Criteria	JORC Code explanation	Commentary
data points	*and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* 2. *Specification of the grid system used.* 3. *Quality and adequacy of topographic control.*	locations surveyed by using a DGPS by either a contractor or staff surveyor. All pre 2005 drill holes were surveyed by either staff surveyor(s) or contractors using a theodolite. All underground drill hole collars are surveyed by company surveyors or contractors using a theodolite. Surveys are entered into the Aeris Resources corporate Acquire database. Underground samples are located spatially against survey stations which are installed by either staff or contract surveyors. 2. Geology interpretations and grade estimates are based on a local Tritton Mine Grid (TMG). The TMG is rotated 8.423º to the west from AGD 66 true north. 3. Quality and accuracy of the drill collars are suitable for geological interpretation and resource estimation. A majority of drill holes intersecting the current Mineral Resources are from underground drill holes.
Data spacing and distribution	1. *Data spacing for reporting of Exploration Results.* 2. *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* 3. *Whether sample compositing has been applied.*	1. Drill spacing across the Tritton deposit vary from approximately 80m (N) x 40m (RL) to 20m (N) x 20m (RL). 2. As a general rule Measured Mineral Resource is defined from a 20m x 20m drill spacing. Indicated Mineral Resource is defined from a 40m x 40m drill spacing. Inferred Mineral Resource is defined from drill spacings up to 100m x 100m. Based on the observed geological continuity from underground develop and drill holes the drill spacing is appropriate. . 3. The Tritton mineralisation is defined sufficiently to define both geology and grade continuity for a Mineral Resource estimation and Ore Reserve evaluation. The material defined as Measured is suitable for detailed stope design. 4. Samples are composited to 1.0 metre intervals. A majority of the assay data are 1.0 metres in length. Within an estimation domain composite lengths are created at 1.0 metre intervals from HW to FW. In some instances the FW sample may be less than 1.0 metre in length. Samples greater than or equal to 0.5 metres are retained for estimation and those less than 0.5 metres are not used for estimation.

Criteria	JORC Code explanation	Commentary
Orientation of data in relation to geological structure	*1. Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *2. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	1. Underground drill holes are collared from dedicated HW drill drives. In some instances drill holes intersecting mineralisation perpendicular to geology. This is more noticeable on the periphery of the deposit and for holes which intersect the deposit down dip at oblique angles. This is not considered to represent a material issue for Measured and Indicated Mineral Resource. There are a small number of holes intersecting mineralisation below the 4000mRL level which cross cut the deposit at an acute angle. Underground samples taken from development headings do not extend across the entire estimation domain. There is potential for a small amount of bias to occur, however it should be noted that there is only a small number of faces sampled per level and the amount of diamond drill data would minimise any potential grade bias. 2. No material issues due to sampling bias have been identified. Based on mine to mill reconciliations over the course of mining activities the Tritton resource estimate reconciles within tolerance levels.
Sample security	*1. The measures taken to ensure sample security.*	1. Chain of Custody is managed by the Company. Samples are stored on site in polyweave bags containing approximately 5 samples. These bags are securely tied, then loaded and wrapped onto a pallet for dispatch to the laboratory. The samples are freighted directly to the laboratory with appropriate documentation listing sample numbers and analytical methods requested. Samples are immediately receipted by a laboratory staff member on arrival, with a notification to Aeris Resources of the number of samples that have arrived.
Audits or reviews	*1. The results of any audits or reviews of sampling techniques and data.*	1. External reviews and audits have been conducted by AMC, Optiro and HDR between 2010 to 2015. No fatal flaws or significant issues were identified.

6.4.2 Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	*1. Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* *2. Data validation procedures used.*	1. All assay results are logged against unique sample numbers. A sampling sheet detailing sample numbers and core / RC intervals is completed prior to sample collection. During the sampling process each sample interval is cross-referenced to the sample number and checked off against the sampling sheet. Pre-numbered bags are used to minimize errors. Assay data is received via email in a common electronic format and verified against the AcQuire database. 2. Data validation and QAQC procedures are completed by staff geologists. Geology logs are validated by the core logging geologist. Assay data is not uploaded to the corporate Acquire database until all QAQC procedures have been satisfied.
Site visits	*1. Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* *2. If no site visits have been undertaken indicate why this is the case.*	1. Brad Cox (Aeris Resources – Geology Manager) has made numerous site visits during the latest resource definition drill program from 2014 onward.
Geological interpretation	*1. Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* *2. Nature of the data used and of any assumptions made.* *3. The effect, if any, of alternative interpretations on Mineral Resource estimation.* *4. The use of geology in guiding and controlling Mineral Resource estimation.* *5. The factors affecting continuity both of grade and geology.*	1. The confidence in the Tritton geology model is high. The deposit has been mined for over 10 years. During this period a significant amount of geological data has been collected from drill core and underground mapping. This information has been used to create the geology models which as each level is developed are showing good correlation between interpreted domain boundaries and their actual location (< 5 metres difference). 2. Data used for the geological interpretation includes drill hole data (diamond core) and underground mapping. There are not significant assumptions made other than the mineralised system extends between drill holes along the interpreted orientation. The geology is relatively simple with minimal structural deformation. Mineralisation is easily visible from the host turbidite sequences. The geometry of the mineralised system is well understood at drill spacings up to 40m x 40m.

Criteria	JORC Code explanation	Commentary
		3. For the updated Mineral Resource estimate two different geological interpretations were trialled. The alternative interpretation domained out 2 high grade (+2% Cu) lodes below 4100mRL. Their orientation is oblique to the dominate trend of the sulphide system. The alterative model was used to understand the grade/metal differences between each interpretation. There was no material difference between the estimates. The high grade domains were discarded from the final estimate with Cu estimated within a lower grade 0.4% Cu shell. 4. Estimation domains used for the latest resource estimate are based on interpreted geology defined from drill core and underground mapping. Cu estimates are constrained within a broad low grade 0.4% Cu shell based on log probability distribution. Internally within this domain unmineralised turbidite sequences are domained out and a massive high pyrite unit along the HW is also modelled separately. A significant sub horizontal fault at ~4050mRL is also modelled and may affect Cu grades either side. Given the stratiform nature of mineralisation variogram continuity is orientated down the plane of the sulphide horizon. Within the plane the direction of maximum continuity is steeply plunging to the south. Structural measurements from orientated drill core have assisted with determining the orientation of ore boundaries in areas of sparse drilling below 4000mRL. 5. Mineralisation is still open at depth below the 3860mRL (> 1,400 metres below surface). Although there is not a significant amount of information the geology (stratigraphy and ore textures) is similar in this region. From 4300mRL down the orientation of mineralisation changes from a NNE trend to a E-W trend. Within this zone mineralisation changes from two distinct mineralised systems, divided by a small unmineralised sequence, to a broad lower grade thicker zone of mineralisation. The change in orientation is not fully understood, however the geometry change is well understood.
Dimensions	*1. The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	1. The main Tritton mineralised zone is tabular in nature with an overall down dip length of 1.5km with mineralisation still open at depth. Mineralisation begins at approximately 155m below surface (5115mRL). The main body varies in thickness averaging 6-8 metres above the main “roll over” at 4500mRL. Below the “roll over” the mineralised sulphide

Criteria	JORC Code explanation	Commentary
		package thickens with true widths in the order of 15 to 30 metres to 4300mRL. Below this the mineralised body dips at a shallower angle (25º) and thickens to 70m thick down to the 4000mRL. The geological understanding below this RL is limited based on a small drill hole dataset and the dimensions of mineralisation are inferred. The strike length of the mineralised system is typically in excess of 300m (5000mRL to 4300mRL). Below this the strike length reduces to approximately 100 to 150 metres. An along strike extension of the Tritton deposit (South Wing) is located on the southern extremities of the central Tritton resource. The south wing is broadly triangular in shape with the long axis down dip with a length of 900 metres with a width at the widest point of 250 metres. The thickness varies from 1 to 8 metres averaging 2 metres.
Estimation and modelling techniques	*1. The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* *2. The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* *3. The assumptions made regarding recovery of by-products.* *4. Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* *5. In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* *6. Any assumptions behind modelling of selective mining units.* *7. Any assumptions about correlation between*	1. Ordinary kriging was used to estimate all variables. Ordinary kriging is an appropriate for this style of mineralisation. Given that a majority of Cu is contained within one domain (0.4% Cu shell) there will be some grade averaging occurring, particularly in areas with variable Cu grades. An indicator kriged estimate was trialled to determine whether some of this variability could be captured in the estimate. There was little difference between the OK and IK estimates. The indicator variograms at cut-offs above the median have short ranges (≤10m) and is likely the reason the IK estimate does not reflect a higher degree of variability. Vulcan software was used to create 3D geology/estimation domain wireframes, generate descriptive statistics and grade estimation. Isatis software was used to report descriptive statistics and model variograms. Metal per composite analysis and review of descriptive statistics were used to determine appropriate top cut values. For the Cu data no top cuts were applied. Estimation was either performed in 2 passes or 3 depending on the search size and dimensions of the estimation domain. Estimation pass 1 was generally set at 70% of the variogram range, estimation pass 2 set at 140% of variogram range and estimation pass 3 was designed to populate all remaining blocks within the estimation domain. A majority of Measured and Indicated Mineral Resource classified blocks are associated with estimation pass 1. 2. All estimates within each estimation domain are validated against declustered composites. Mean grade estimates that fall within 5% of the

Criteria	JORC Code explanation	Commentary
	variables. 8. *Description of how the geological interpretation was used to control the resource estimates.* 9. *Discussion of basis for using or not using grade cutting or capping.* 10. *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	declustered composite mean grade are considered acceptable. If the difference is outside a 5% tolerance then the estimation and/or decluster cell size is reviewed and changes made if necessary. The model is also reconciled against previous models and mill reconciled data on 6 monthly increments. Estimates are within acceptable tolerance levels when compared against the reconciliation data. 3. No assumptions have been made for the recovery of gold and silver by-products. 4. Other variables estimated included S, Fe, Zn and bulk density. Sulphur estimates are used for the identification of PAF material. 5. The parent block sized used for the updated estimate was 10m (E) x 10m (N) x 4m (RL) with sub celling down to 1m (E) x 1m (N) x 1m (RL). The cell size takes into consideration drill spacing (grade control 20m x 20m x 20m and resource definition 40m x 40m x 40m) and grade variability in different orientations. 6. No assumptions have been applied to the model for selective mining unit. 7. No correlation has been made between variables. fusion 8. The distinction between background Cu and Cu associated with mineralisation was defined from a combination of geology/textural logging and population distributions associated with a log probability plot. From this a 0.4% Cu cut-off was selected to define the bounding Cu estimation domain. Geological domains were modelled and tested against each other (geological interpretation, descriptive statistics, QQ plots and contact plots) to determine whether they could be incorporated into one domain or separated. This approach was used for each variable estimated. Generally domain boundaries were treated as hard domains whereby only composite data associated with an estimation domain is used for estimation. In some instances, based on contact plots, if a semi-soft profile is identified across an estimation domain boundary then composites from an adjoining estimation domain can be selected for estimation. 9. Each estimation domain for each variable was reviewed to determine whether top cuts are required. Top cuts were applied based on metal per composite analysis, histogram distributions and spatial location of composite data. Top cuts were applied if too much metal was assigned to particular composites (metal per composite) and/or clear disconnect from

Criteria	JORC Code explanation	Commentary
		histogram distribution and spatially where the anomalous composites occur in relation to other samples. 10. All estimates within each estimation domain are validated against declustered composites. Mean grade estimates that fall within 5% of the declustered composite mean grade are considered acceptable. If the difference is outside a 5% tolerance then the estimation and/or decluster cell size is reviewed and changes made if necessary. Estimates were also validated visually in Vulcan displaying block estimates and composite data. Swath plots on 20m levels were also created showing block estimates and declustered composite data in the X, Y and Z directions for each variable estimated.
Moisture	*1. Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	1. Tonnages are estimated on a dry basis.
Cut-off parameters	*1. The basis of the adopted cut-off grade(s) or quality parameters applied.*	1. A 0.4% Cu cut-off was used for domaining mineralised Cu. The selection of an appropriate cut-off grade was based on geology (ore textures and lithology) and log probability plot distributions. Previously a higher cut-off was used (0.8% Cu) which reflected the higher grade more constrained geometry of the mineralised system. The mineralised system below the current mining front is becoming thicker with less pronounced higher grade zones of mineralisation.
Mining factors or assumptions	*1. Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	1. The only consideration to the mining method is the minimum interpretation width applied is 2 metres downhole. Otherwise no other mining assumptions have been applied to the Tritton model.
Metallurgical	*1. The basis for assumptions or predictions regarding*	1. The dominant Cu mineral within the Tritton deposit is chalcopyrite.

Criteria	JORC Code explanation	Commentary
factors or assumptions	*metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Material mined from Tritton is processed at the Tritton Copper Operations copper ore processing plant. Copper recovery to copper concentrate at a 24% copper in concentrate grade is on average 94.5%.
Environmental factors or assumptions	1. *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	1. Tailing waste from ore processing is disposed at the current tailings storage facility within ML1544 (or utilised as paste fill). Waste from underground development is stored on site for future rehabilitation of the Tailing Storage Facility. Any potentially acid forming waste is used for stope backfill underground. No significant environmental impacts have been identified from the Tritton mining operation.
Bulk density	1. *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* 2. *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.* 3. *Discuss assumptions for bulk density estimates used*	1. Bulk density has been estimated via OK within all estimation domains. For the background estimation domain outside of the mineralised system two estimation passes were run. For unestimated blocks outside of the 2 estimation passes a default value of 2.90 was applied (mean value from internal dilution estimation domain). 2. Bulk density values were measured using the Archimedes Principle Method' (weight in air v's weight in water). Varying forms of silicification is present throughout the mineralised system and porosity associated with the turbidite host sediments is negligible. Vugs have been noticed within the drill core on rare occasions. Technically the bulk density determination method does not take into account for the presence of

Criteria	JORC Code explanation	Commentary
	in the evaluation process of the different materials.	vugs. Given they have only been observed on the rare occasion and are not correlatable to specific zones they are not considered to represent a material problem with current bulk density determinations. 3. Bulk density has been estimated from the bulk density measurements. For material outside the mineralised domains an average density value for the host material has been assigned based on the mean bulk density from the internal dilution estimation domain.
Classification	*1. The basis for the classification of the Mineral Resources into varying confidence categories.* *2. Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* *3. Whether the result appropriately reflects the Competent Person's view of the deposit.*	1. Classification of the resource estimate has been guided by confidence in the geological interpretation, drill density, underground development. Measured classified areas were constrained to levels defined from grade control drilling (drill spacing 20m x 20m x 20m). The Measured resource extends down to the 4170mRL level. Indicated classified areas were constrained to 40m x 40m drill spacings below 4170mRL. The Indicated resource extends down to the 4000mRL level. The Inferred Mineral Resource incorporates the south wing estimation domain (located along strike and south of the main Tritton mineralised system) and down dip extensions below the Indicated resource within the main Tritton mineralised system. Within the main mineralised system the Inferred resource was extended down to the 3860mRL level which coincides with the deepest drill intersection. 2. The drill and input data density is comprehensive in its coverage for this style of mineralisation and estimation techniques to allow reasonable confidence for the tonnage and grade distribution to the levels of Measured, Indicated and Inferred. 3. The updated Tritton geology interpretation/model and resource estimate appropriately reflects the competent persons understanding of the geological and grade distributions. The classification of the resource in the area of the upper Tritton Pillars has been downgraded from Measured to Indicated due to concerns regards the continuity of this mineralisation around old and unfilled stopes.
Audits or reviews	*1. The results of any audits or reviews of Mineral Resource estimates.*	1. External reviews and audits have been conducted by AMC and Optiro for early generations of the Tritton resource models. No fatal flaws or significant issues with the past Tritton models were identified at the time. The current geological interpretation, estimation domain assumptions and

Criteria	JORC Code explanation	Commentary
		grade estimates have been reviewed by HDR. No fatal flaws or significant issues were identified.
Discussion of relative accuracy/ confidence	1. *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* 2. *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* 3. *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	1. The models have been validated visually against drilling and statistically against input data sets on a domain and on swath plot basis. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC code. Over a 12 month period the Measured Mineral Resource should reconcile within 5% of reported mill figures. This trend has been consistently observed our previous 12 month periods. 2. The statement relates to local estimates of tonnes and grade above 4170mRL for Measured material. Below 4170mRL the estimate is treated as a global estimate for Indicated material. For the Indicated material grade control drilling to nominal 20m x 20m drill spacing will be required to firm the mineralised position and grade distribution suitable for final stope designs. Inferred material relates to a global estimate. 3. Mine to mill reconciliations for the FY2016 year have shown that Ore Reserves has estimated within 2% of tonnes and 2% of grade providing a minimal variance for metal. Tritton resource has been mined since 2005. Reconciliations demonstrate the current models provide good confidence in the estimation and the estimation process used for the Tritton Resource.

7 ORE RESERVE ESTIMATE

7.1 RESULTS

The Tritton mine Ore Reserve Estimate as at 30th June 2016 is reported in **Table 5**. It is reported according to JORC 2012.

Table 5 Ore Reserve Estimate for Tritton deposit as at 30 June 2016

Category	Tonne (k tonne)	Copper %	Contained Copper (k tonne)
Proved	3,580	1.7	61
Probable	2,790	1.4	39
Total	**6,370**	**1.6**	**100**

1. Ore Reserves are reported as INCLUSIVE of the supporting Mineral Resource estimate
2. Discrepancies in summation will occur due to rounding

7.2 CHANGES FROM PREVIOUS ESTIMATE

The Ore Reserve estimate presented in this report is an update that accounts for changes to the Mineral Resource estimate including depletion due to mining in the year since last report. An increase in the Mineral Resource, net of depletion, resulted from a resource drilling program and subsequent geology modelling of the deposit. Measured and Indicated Mineral Resource has been extended to 4000mRL.

The Ore Reserve has been extended to the depth of 4050mRL consistent with the extension of the Indicated Mineral Resource to 4000mRL. None of the available Mineral Resource below 4050mRL was converted to Ore Reserve, principally due to insufficient grade.

All of the Measured and Indicated Mineral Resource has been assessed for inclusion in the Ore Reserve. All resource that can be converted has been reported as Ore Reserve. Conversion rates of resource to reserve are 80% for that material above 4080mRL and 5% for that material below 4080mRL, (this level is the last of sublevels where high rates of conversion is possible with current methods).

Modifying factors applied for dilution and ore loss have been slightly altered from the prior estimate where the estimate now includes some larger stopes. The modifying factors are selected following review of production reconciliation against the Ore Reserve estimate. The reconciliation indicates that the Ore Reserve estimate is within 2% of the actual ore processed for the stopes mined in the year 2015.

The previous Ore Reserve estimate was made as at June 30th 2015.

Table 6 Change in Ore Reserve from previous estimate

Estimate	Category	Tonne (k tonne)	Copper %	Contained Copper (k tonne)
June 2016	Proved	3,580	1.7	61
	Probable	2,790	1.4	39
	Total	**6,370**	**1.6**	**100**
June 2015	Proved	2,359	1.8	42
	Probable	2,040	1.7	34
	Total	**4,399**	**1.7**	**76**
Difference	***Proved***	***+1220***	***-0.1***	***+19***
	Probable	***+750***	***-0.3***	***+5***
	Total	***+1970***	***-0.1***	***+24***

7.3 STATEMENT OF COMPLIANCE WITH JORC CODE REPORTING

This Ore Reserve statement has been compiled in accordance with the guidelines defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves.

7.3.1 Competent Person Statement

I, Ian Sheppard, confirm that I am the Competent Person for the Tritton mine Ore Reserve section of this Report and:

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code, 2012 Edition, having five years' experience that is relevant to the style of mineralisation and type of deposit described in the Report and to the activity for which I am accepting responsibility.
- I am a Member of The Australasian Institute of Mining and Metallurgy, No. 105998.
- I have reviewed the Report to which this Consent Statement applies.

I am a full time employee of Aeris Resources Limited.

I have disclosed to the reporting company the full nature of the relationship between myself and the company, including any issue that could be perceived by investors as a conflict of interest. Mr Sheppard has disclosed to the reporting company the full nature of the relationship between himself and the company, including any issue that could be perceived by investors as a conflict of interest. Specifically Mr Sheppard has rights to 22,418,546 share options that will vest over the next five years and may be converted to shares over time when various conditions are met.

I verify that the Ore Reserve section of this Report is based on and fairly and accurately reflects in the form and context in which it appears, the information in my supporting documentation relating to the Ore Reserve estimate.

7.3.2 Competent Person Consent

With respect to the sections of this report for which I am responsible – Tritton Mine Ore Reserve Estimate - I consent to the release of the Mineral Resources and Ore Reserves Statement as at 30 June 2016 for Tritton mine.

Signature of Competent Person Ian Sheppard Member No.105998 AusIMM Ian Shepp	Date 01 / 08 / 2016
Signature of Witness	Witness Name and Address Narelle Wynn Lutwyche Q 4030

7.4 EXPERT INPUT

A number of persons have contributed key inputs to the Ore Reserves determination. These are listed below.

In compiling the Ore Reserve the Competent Person has reviewed the supplied information for reasonableness, but has relied on this advice and information to be correct.

Table 7 Expert contribution to Ore Reserve

Expert Person / Organization	Area of Expertise
Brad Cox	Mineral Resource geology and resource estimating block Model
Wayne Race	Detailed stope design
Peter Erepan	Metal recovery in ore processing

7.5 JORC CODE, 2012 EDITION – TABLE 1 REPORT: TRITTON ORE RESERVE

7.5.1 Section 4 Estimation and Reporting of Ore Reserves

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	1. *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* 2. *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	1. The Ore Reserve estimate is based on the 30th June 206 Mineral Resource for Tritton mine, estimated by the Tritton Resource named *Model trifeb16_rsc-12032016.bmf.* Mr Brad Cox is the competent person responsible for Mineral Resource Estimation and both estimating models. Measured Mineral Resource is estimated above 4170mRL and Indicated Mineral Resource below this level down to 4000mRL. 2. Mineral Resources are quoted as INCLUSIVE of the Ore Reserve estimate
Site visits	1. *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* 2. *If no site visits have been undertaken indicate why this is the case.*	1. Mr Ian Sheppard, competent person for the Tritton mine Ore Reserve, has visited the Tritton mine on several occasions and is familiar with the mine conditions.
Study status	1. *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* 2. *The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	1. Tritton mine Ore Reserve estimate is based on ten years of mine production history, production budgets, and mine designs that in aggregate exceed the level of detail expected from a feasibility study. The mine budget and associated Life of Mine plan demonstrate the technical and economic viability of mining the Ore Reserve. 2. Modifying factors used in the conversion of Mineral Resource to Ore Reserve are based on reconciliation and observation of past mining and ore processing performance.
Cut-off parameters	1. *The basis of the cut-off grade(s) or quality parameters applied.*	1. The June 2016 Ore Reserve uses copper grade, Cu%, as the cut-off grade criteria. 2. A cut-off grade of 1.1% Cu is applied to whole stope estimates of grade after dilution. Stopes are designed within the Mineral Resource grade envelope that has been interpolated by geologists at a nominal 0.6% Cu cut-off. Designers aim to reject as much mineralisation with grade less than 1.1% Cu as is practical from the stope, however sub-

Criteria	JORC Code explanation	Commentary
		cut-off grade mineralisation will be included if necessary to generate a practical stope design. The average grade of the whole stope volume is estimated to give the pre-dilution stope tonnage and grade, (including any sub cut-off grade blocks within the stope). Dilution from surrounding rock and from backfill is then estimated followed by estimation of ore loss. Dilution and ore loss factors are applied to estimate the diluted stope grade. The diluted whole of stope grade is tested against the cut-off grade. The stope average diluted grade must exceed the 1.1% Cu cut-off grade to be accepted. 3. Where access development tunnel designs are available, all Mineral Resource inside these development design shapes and above 0.6% Cu is converted directly to Ore Reserve without modification. A lower marginal cost applies to this material equivalent only to the cost of ore processing. Mining costs will be incurred irrespective of a decision to process this material or not. Hence a lower cut-off grade of 0.6% Cu is applied. No dilution or ore loss factors are applied to Mineral Resource contained within the development shapes in the estimation of Ore Reserve. 4. Gold and silver grades in the ore are of minor importance as economic by-products. Gold and silver grades are strongly correlated with copper grade and this combined with minor economic importance means they need not be included in the cut-off grade criteria. Gold in copper concentrate grades are only occasionally above the payable limit of 1.0g/t. Silver in concentrate grades are approximately 60g/t and so silver contributes a modest value of AUD$40 to $50 per tonne copper concentrate. 5. There are no significant impurities in the mineralisation that require inclusion in the cut-off grade criteria.
Mining factors or assumptions	*1. The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* *2. The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including*	1. June 2016 Mineral Resources have been converted to; underground Ore Reserve by a process of detailed stope and development design. The life of mine plan scheduled production is equivalent to the Ore Reserve. 2. The mining method used at Tritton mine is underground open stoping with cemented paste backfill. Open stope mining methods have been used with success for ten years. Use of cemented paste fill allows high rates of conversion of Mineral Resource to Ore Reserve, with no permanent pillars required to be left. 3. Geotechnical stability of the stope designs is based on stable span dimensions

Criteria	JORC Code explanation	Commentary
	associated design issues such as pre-strip, access, etc. 3. *The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.*	established over several years of operational experience with the use of cemented paste fill. A modest level interval of 20m vertical is used to limit the length of hanging wall exposure in the shallow dipping (35 to 50 degree) ore body. Tritton specific empirical design curves based on prior stope stability are used to assist with design of stable spans.
	4. *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).*	4. The Ore Reserve estimates for development and stope ore include the volume of material that is below the cut-off grade and which is considered impractical to exclude from the surrounding or adjacent volume of ore. Such diluting material is inclusive to the design ore volume and estimate of grade.
	5. *The mining dilution factors used.* 6. *The mining recovery factors used.* 7. *Any minimum mining widths used.* 8. *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* 9. *The infrastructure requirements of the selected mining methods.*	5. Ore recovery factor of 90% and dilution factor of 11% are applied in the estimation of Ore Reserve for stopes less than 40m high; “small stopes”. 6. Ore recovery factor of 95% and dilution factor of 5% are applied in the estimation of Ore Reserve for the largest stope 40m or higher 7. Ore recovery factor of 50% and dilution factor of 20% are applied in the estimation of Ore Reserve for the upper levels old pillar stopes. 8. Dilution due to over break of the hanging wall of small stopes is estimated as an average of 12 % for small stopes. A copper grade of 0.8% Cu is estimated for this dilution, based on the results of stope reconciliation. 9. Dilution due to fall-off of paste fill from adjacent filled stopes is estimated as an average of 3.0% for all stopes. There is no economic copper in the paste fill dilution. 10. Ore loss due to under break on the footwall of the small stopes, (due the shallow dip) is estimated as an average of 12% for all stopes. The grade of this ore loss is assumed to be the average of the un-diluted stope grade. 11. Ore loss due to inability to recover all the broken ore is estimated at an average of 2% for all stopes. The grade of this ore loss is assumed to be the un-diluted stope grade. 12. The detailed modifying factors described in items 8 to 11 above are simplified into the simple 90% ore recovery and 11% dilution factors applied in the Ore Reserve estimate,

Criteria	JORC Code explanation	Commentary
		giving the same estimate within precision of the estimate 13. Inferred Mineral Resources is scheduled within the Life of Mine plan for Tritton, however the small quantity of inferred material does not affect the economic viability of the Ore Reserve. All Inferred Mineral Resource is schedule for production after the Ore Reserve is exhausted and does not impact the decision to mine the Ore Reserve material. 14. Capital development, ventilation, backfill distribution, electrical, pumping and other infrastructure necessary to support the Tritton mine is installed incrementally over time. The sustaining capital cost of installing the infrastructure is included in the Life of Mine plan.
Metallurgical factors or assumptions	*1. The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* *2. Whether the metallurgical process is well-tested technology or novel in nature.* *3. The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* *4. Any assumptions or allowances made for deleterious elements.* *5. The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* *6. For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	1. The Triton mine ore is treated at the existing Tritton ore processing plant located adjacent to the mine portal. Copper, gold and silver metal are recovered to a copper concentrate by sulphide flotation methods. 2. The sulphide flotation treatment method is proved on Tritton ore with over 12 million tonne of ore successfully treated to date. 3. Tritton ore processing plant to produces a copper concentrate with 24% copper. Average recovery ranging from 94% to 95% of copper is achieved. Gold is recovered to the copper concentrate at 45% recovery, however grades in the concentrate are generally below payable limits and only occasional value is derived from the gold. Silver recovery averages 75%. 4. The Ore Reserve assumes that no allowances are required for deleterious elements in the copper concentrate. This is supported by historical production of a very clean concentrate.
Environmetal	*1. The status of studies of potential environmental impacts of the mining and processing operation. Details of waste*	1. The Tritton deposit is located on ML1544. The mine is fully permitted for production. 2. Tailing from ore treatment are disposed to the existing Tritton Resources tailing storage

Criteria	JORC Code explanation	Commentary
	rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.	facility. Closure of this tailing storage facility will be required at end of mine life. Sufficient topsoil and waste rock with suitable geochemistry is stockpiled and available for capping for capping of the facility at mine closure. 3. Waste rock with potential to be acid forming is disposed into stopes underground and not stored on surface.
Infrastructure	*1. The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	1. The Tritton mine and ore processing site has all necessary infrastructure installed and operating. Infrastructure includes change facilities, offices, workshops, electrical power, water, and road access. Sufficient skilled labour is available in region to support the mine and accommodation is available in the town of Nyngan located within 50km distance from the mine. Land from which the Tritton mine is accessed is freehold lease owned by Tritton Resources Pty Ltd.
Costs	*1. The derivation of, or assumptions made, regarding projected capital costs in the study.* *2. The methodology used to estimate operating costs.* *3. Allowances made for the content of deleterious elements.* *4. The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.* *5. The source of exchange rates used in the study.* *6. Derivation of transportation charges.* *7. The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* *8. The allowances made for royalties payable, both Government and private.*	1. Capital costs for the Tritton mine include only sustaining capital for mine development, ventilation extension and mining equipment replacement. These costs are based on recent development experience and the purchase of similar mine equipment. Accuracy of estimate is at feasibility study or better precision, (± 15%). The sustaining capital expenditure schedules are included in the Life of Mine plan. 2. Tritton mine operating cost estimates are based on recent experience applied to first principles build-up from physical schedules for the budget year (FY2017 - ending June 2017). The budget estimates are projected forward with appropriate modification to account for increasing depth of mining over time. Accuracy beyond the budget year is considered to be ±15%. 3. Metal price assumptions for copper, gold and silver are Aeris Resources corporate long term assumptions derived from a variety of market sources – see next section. 4. Exchange rates used in the studies that support the Ore Reserve estimate are Aeris Resources corporate long term assumptions derived from a variety of market sources – see next section. 5. Copper concentrate product transport costs include road and rail freight to port, port handling and sea freight. The costs assumed in the Life of Mine plan are based on the budget year contract rates with future changes based on market intelligence. Budget for

Criteria	JORC Code explanation	Commentary
		financial year 2016 costs are approximately AUD$90 per dry tonne concentrate. 6. Copper concentrate treatment and refining charges assumed in the Life of Mine plan are the financial year 2016 budget costs; USD$100/t concentrate smelting and USD 10c/lb copper refining, 7. NSW government royalty of 4% is payable on revenue less deductible items. After deductions, the effective royalty rate on revenue is approximately 3% for Tritton Resources. No private royalties will apply.
Revenue factors	*1. The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* *2. The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	1. Tritton Ore Reserve breakeven cut-off grade is calculated using the mid-term (2018) Aeris Resources forward looking economic assumptions regards metal price, exchange rate, smelter treatment, and product handling cost: a. Copper price of USD$5,200/tonne b. Gold price of USD$1200/oz c. Silver price of USD$17/oz d. AUD:USD exchange rate of 0.71 e. Copper treatment charge of USD$100/tonne f. Copper refinery charge of USD10c/lb g. Standard Tritton Resources contract smelter terms for payable metal; effective copper payable is 95.8% for concentrate with 24% copper content h. Assumptions were current at June 2016 Under this range of economic assumptions and the estimated operating costs, the break-even grade varies from; • 1.4% Cu if full site costs are included • 1.1% Cu if only variable costs are considered (site fixed administration cost ignored), and cost reduction from a change to larger stopes Based on the above estimated range of break-even grades, a cut-off grade of 1.1% Cu has been applied in the estimation of Ore Reserve. Prior year cut-off grade was 1.2% Cu. In general the shallow small stopes in the Ore Reserve have been designed to this slightly higher cut-off grade. The cut-off grade policy applied in the estimate of Ore Reserves is derived by testing the value of the whole Tritton Operations business at a range of design cut-off

Criteria	JORC Code explanation	Commentary
		grades. The selected cut-off policy of 1.1% Cu was shown to return the best value given the assumed forward curve for copper price.
Market assessment	*1. The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* *2. A customer and competitor analysis along with the identification of likely market windows for the product.* *3. Price and volume forecasts and the basis for these forecasts.* *4. For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	1. The world market for copper concentrate is large compared to production from Tritton mine. The Tritton mine copper concentrate is a very clean product with low impurities and demand for this product from copper smelters is expected to remain high. All copper concentrate is sold under life of mine contract to Glencore International AG.
Economic	*1. The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.* *2. NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	1. The Tritton Life of Mine plan and associated commercial model estimates a positive Net Present Value for the operation at a discount rate of 7%. The economic assumptions used in the valuation of the Life of Mine plan vary over time. They are consistent with the assumptions of economic inputs applied in the calculation of break-even grade discussed above. 2. The Tritton mine is one of several mines that will supply ore to the Tritton processing plant in the Life of Mine plan. The plan assumes that Tritton mine shares the cost of site administration, processing plant sustaining capital and other overheads with the other mines.
Social	*1. The status of agreements with key stakeholders and matters leading to social licence to operate.*	1. The Tritton mine is located on existing Mining Lease ML1544. The mine is fully approved to operate. 2. Tritton Resources is based in the township of Nyngan in the Bogan Shire NSW. Strong community support for the continued operation of Tritton Resources has been evidenced in regular community consultation sessions. There are no known objections from the community against the Tritton Resources operations. Tritton Resources owns the land on which access to Tritton mine is located.
Other	*1. To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore*	1. No material natural risks have been identified for the Ore Reserves. 2. All copper concentrate produced by Tritton Resources from the Tritton mine will be sold to Glencore International AG under an existing life of mine contract.

Criteria	JORC Code explanation	Commentary
	Reserves: 2. *Any identified material naturally occurring risks.* 3. *The status of material legal agreements and marketing arrangements.* 4. *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	
Classification	1. *The basis for the classification of the Ore Reserves into varying confidence categories.* 2. *Whether the result appropriately reflects the Competent Person's view of the deposit.* 3. *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	1. The Proved Ore Reserve estimate results from the conversion of Measured Mineral Resource. The end of the Measured Mineral Resource for June 2016 is set at 4170mRL, which is the limit of completed grade control drilling. Above 4170mRL is Proved Ore Reserve and Probable Ore Reserve is below this level. 2. Below 4170mRL all Ore Reserve is categorized as Probable. This Ore Reserve is based on the conversion of Indicated Mineral Resource described by the resource model. 3. A Probable Ore Reserve of 0.27Mt has been estimated by conversion of blocks of resource remaining as pillars between completed primary stopes that were mined before the operation used cemented backfill. These blocks of pillar resource are located in the upper levels of the mine; 4860mRL and above. The pillar Ore Reserve is derived from Indicated Mineral Resources. Uncertainty over the geotechnical condition of the rock mass in the pillar resource would have been applied as a modifying factor in the estimation of the pillar Ore Reserve. Only Probable Ore Reserve would be estimated for the pillars, irrespective of the resource categorization. 4. The classification of the Ore Reserve as a combination of Proved and Probable is an

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>appropriate reflection of the conditions in Tritton mine in the opinion of the competent person, Mr Ian Sheppard.</td></tr>
<tr><td><i>Audits or reviews</i></td><td><i>1. The results of any audits or reviews of Ore Reserve estimates.</i></td><td>1. No audits of this June 30th 2016 Ore Reserve have been completed. Previous Ore Reserve estimates have been externally reviewed as part of requirements for provision of finance with no significant discrepancies found.</td></tr>
<tr><td><i>Discussion of relative accuracy/ confidence</i></td><td><i>2. Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.</i>
<i>3. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>
<i>4. Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.</i>
<i>5. It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where</i></td><td>1. For Tritton mine;
<table>
<tr><th>Criteria</th><th>Risk Rating</th><th>Comment</th></tr>
<tr><td>Mineral Resource estimate for conversion to Ore Reserves</td><td>Low</td><td>Reconciliation of the Mineral Resource and Ore Reserve shows good correlation between actual and estimated; <5% difference on tonne, Cu grade and contained Cu metal for Proved Ore Reserve. The resource modelling that supports Indicated Mineral Resource estimates has been shown to be moderately conservative after reconciliation with modelling that supports Measured Mineral Resource (based on greater drilling density).</td></tr>
<tr><td>Classification</td><td>Low</td><td>All Probable Ore Reserve based on Indicated Mineral Resource. No complications from modifying factors.</td></tr>
<tr><td>Site visit</td><td>Low</td><td>Site visits completed. Tritton is an operating mine with 10 years production history.</td></tr>
<tr><td>Study status</td><td>Low</td><td>Ore Reserves are support by Life of Mine plan and budgets that are higher precision than Feasibility Study.</td></tr>
<tr><td>Cut-off grade</td><td>High</td><td>Cut-off grade is sensitive to mine operating costs achieved and dilution in addition to the normal metal price volatility risk.</td></tr>
<tr><td>Mining factors</td><td>Medium</td><td>Dilution and ore loss factors are derived from detailed stope review and reconciliation of actual to reserve estimate</td></tr>
<tr><td>Metallurgy factors</td><td>Low</td><td>Tritton ore has been processed for ten (10) years achieving metal recoveries and concentrate quality</td></tr>
</table></td></tr>
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<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td><i>available.</i></td><td>
<table>
<tr><td></td><td></td><td>consistent with those assumed in the preparation of the Ore Reserve.</td></tr>
<tr><td>Environmental</td><td>Low</td><td>Located on existing Mining Lease with all approvals in place.</td></tr>
<tr><td>Infrastructure</td><td>Low</td><td>All required significant infrastructure is in place.</td></tr>
<tr><td>Costs</td><td>Low</td><td>Estimates are based on recent operating cost experience.</td></tr>
<tr><td>Revenue Factors</td><td>High</td><td>Copper metal price has high annual variability. Tritton mine cash margins after sustaining capital are moderate and operations could be suspended during periods of extended low metal price.</td></tr>
<tr><td>Market assessment</td><td>Low</td><td>Life of mine concentrate sale contract is in place.</td></tr>
<tr><td>Economics</td><td>High</td><td>Risk reflects impact of metal price variability and modest grade of the deposit for a deep underground mine.</td></tr>
<tr><td>Social</td><td>Low</td><td>Continued operation of the Tritton Mine is strongly supported by the local community at Nyngan.</td></tr>
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</td></tr>
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End Report